



Mitigation of Switching Overvoltages due to Energization Procedures in Grid-Connected Offshore Wind Farms

Eman A. Awad¹, Ebrahim A. Badran², and Fathi M. H. Youssef³

Research Assistant, Electrical Engineering Department, Faculty of Engineering, Mansoura Univ., Mansoura, Egypt¹

Associate Professor, Electrical Engineering Department, Faculty of Engineering, Mansoura Univ., Mansoura, Egypt²

Professor, Electrical Engineering Department, Faculty of Engineering, Mansoura Univ., Mansoura, Egypt³

ABSTRACT: This paper presents the mitigation of switching overvoltages which are generated due to energization procedures in grid-connected to off-shore wind farms. Pre-insertion resistor, controlled switching of circuit breaker, shunt reactor, or surge arresters are used as protective devices to mitigate energization overvoltages. Alternating Transient Program (ATP) is used in this study for simulating of the test power system and the mitigation methods. The comparison between the four mitigation methods in limiting overvoltage in the power system is introduced.

Keywords: Switching Overvoltage, Wind Turbine, Mitigation, DFIG, ATP.

I. INTRODUCTION

Wind farms are usually found in more remote places where the feeders are long and operated at a medium voltage level [1]. Isolated wind farms away from the main grids are considered weak grids because of long feeders [2]. One of the major concerns in wind farms restoration is the occurrence of the overvoltages as a result of switching procedures [3]. Wind turbine systems are subjected to many forms of transient phenomena brought about essentially by sudden changes in the steady state values of voltages or currents. Such changes may be the result of a lighting stroke, some malfunctions of the system, or be brought about by the switching of a circuit either to clear fault or as a normal operation procedure [4-6].

The switching overvoltage (SOV) are has low front transient which are highly damped, and last for a short duration (few milliseconds or less) [7]. They could occur during energization and disconnection in normal operation or during a fault [8]. The magnitude and shape of the SOVs vary with the system parameters and network configuration. Even with the same system parameters and network configuration, the SOVs are highly dependent on the characteristics of the circuit breaker operation and the point-on-wave where the switching operation takes place [3].

The severity of energization SOV depends on the difference between the supply and the transmission system voltages at the instant of energization [9]. When a transmission system is energized SOV are generated not only on the transmission system but also in the supply network [10]. Pre-insertion resistor (PIR), controlled switching of circuit breaker, shunt reactor, and surge arresters are used as protective devices to mitigate energization overvoltages.

The use of doubly-fed induction generator (DFIG) is receiving an increased attention for wind generation purposes [9, 11]. DFIG is basically a standard, wound rotor induction machine with its stator windings directly connected to the grid and its rotor windings connected to the grid by electronic converters through slip rings, as shown in Fig. 1 [12].

DFIG is one of the most commonly used technologies nowadays, as these offer advantages such as the decoupled control of active and reactive powers and maximum power tracking. These capabilities are possible due to the power electronic converters used in this type of generator [13].

In this paper, the mitigation of SOVs, which are generated due to energization procedures in grid-connected off-shore wind farms, are evaluated. PIR, controlled switching of circuit breaker, shunt reactor, and surge arresters are used as

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

2. The HV, 132 kV, three-phase single-core sea and land cables are modeled as symmetrical, distributed parameter and lumped resistance models.
3. The wind farm transformers are modeled using HYBRID transformer model [14].
4. The rows B, C, and D are modeled as one three-phase single-core cable because they are connected in parallel. Also, the rows E, F, G, and H are modeled in the same way.
5. Only row A is modeled in details.

Fig. 3 shows the nine identical wind turbine transformers (WTTs) in row A. To reduce the simulation time, the complexity of the wind farm model is reduced by equivalent models. The WTGs in the wind farm are aggregated into a three separate equivalent model and the rest of the turbines in row A are modeled as very light loads connected on the LV side of the WTTs. The light load is modeled as a high resistance of 1200 Ω . Therefore, the nine WTTs of row A are considered as transformers under no-load. WTGs are considered as operating on an equivalent internal electrical network provided that the incoming wind velocity is identical or similar on all the WTs [16].

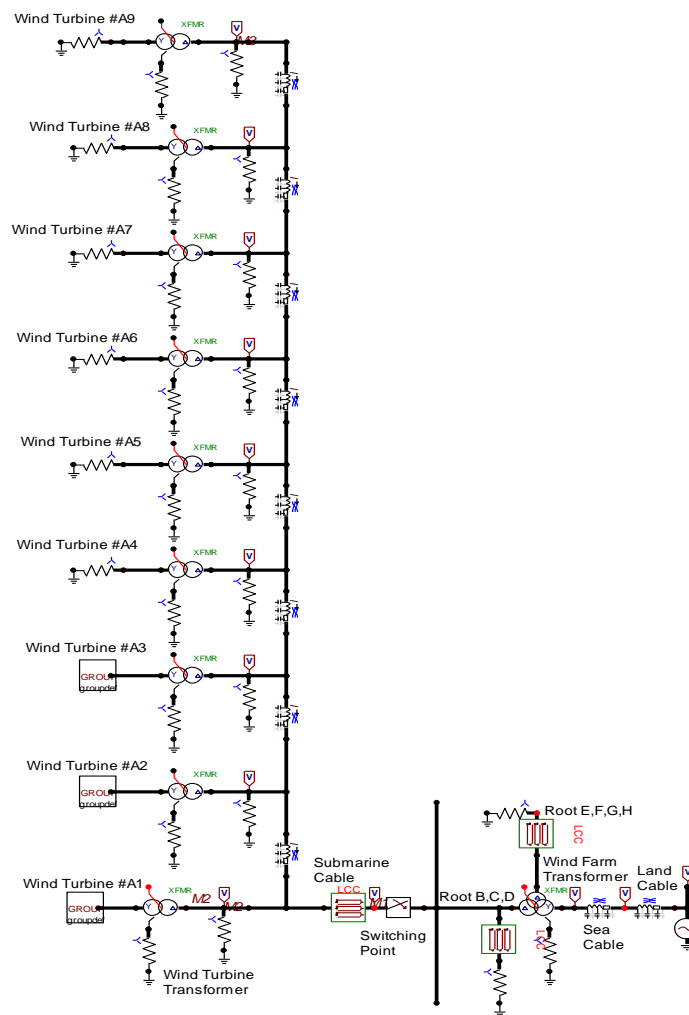


Fig. 3: The offshore wind farm ATP model



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

C. Modeling of Cables and Transformers

The MV single-core submarine cables are the most distinctive electric component in the off-shore wind farms. The 33 kV three-phase single-core submarine cables connect between the HV sides of the WTTs. The geometric configuration of the submarine cables which is calculated based on the power transferred through them [16], and the cable calculated parameters are given in Table 1.

In submarine cables, the armor is usually quite thick. Therefore, it is assumed in this study that, an armor of 5 mm steel wires thickness and a 5 mm outer insulation thickness are incorporated into the three-phase single-core submarine cable design. So, the overall outer diameter of the medium voltage single-core submarine cable is 65 mm. The MV (33 kV) single-core submarine cables are modeled using the frequency dependent LCC model [14]. This model represents the frequency dependence of single-core submarine cable parameters, so this model is much recommended for the electromagnetic transient studies [14].

The sea and land cables are modeled using the three phase Clark model [14] to avoid the numerical errors due to the long length of the HV cables. The model parameters are calculated from the cable dimensions and its materials using distributed parameters of three phase transposed model at 50 Hz. Both dimensions and materials of the HV sea and land cables are taken from [17]. Table 2 gives the positive and the zero sequence resistances, the inductive reactance and the capacitive reactance of the 132 kV land and sea cables, respectively.

Both wind farm transformers and off-shore wind farm transformer are modeled using the HYBIRD transformer model. The wind turbine transformers of row A are modeled using three phase, two windings, HYBIRD model. The wind farm transformer is modeled as three winding transformer using the HYBIRD model, which is suitable for low and medium frequency transient studies [18, 19]. Table 3 gives the data required for transformers modeling.

Table 1: Dimensions of the 33 kV Single-Core submarine Cable

Cross section of conductor [mm] ²	240.0
Diameter of conductor [mm]	18.1
Insulation thickness [mm]	8.0
Diameter over insulation [mm]	35.7
Cross section of screen [mm] ²	35.0
Outer diameter of cable [mm]	45.0

Table 2: The 132 kV Single Core Cables Data

The 18.3 km/ 132 kV land cable (equivalent PI section model)	
+ve sequence resistance	0.087 [m ohm/m]
+ve sequence inductive reactance	0.123 [m ohm/m]
+ve sequence capacitive reactance	9.092 [M ohm*m]
zero sequence resistance	0.1865 [m ohm/m]
zero sequence inductive reactance	0.0551 [m ohm/m]
zero sequence capacitive reactance	9.0915 [M ohm*m]
The 10.5 km / 132 kV sea cable (equivalent PI section model)	
+ve sequence resistance	0.0864 [m ohm/m]
+ve sequence inductive reactance	0.123 [m ohm/m]
+ve sequence capacitive reactance	9.0915 [M ohm*m]
zero sequence resistance	0.1827 [m ohm/m]
zero sequence inductive reactance	0.0619 [m ohm/m]
zero sequence capacitive reactance	9.0915 [M ohm*m]

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

Table 3: Wind Farm and WT Transformers Data

Wind Turbine Transformers Model	
Connection method	Y / Δ
Voltage	0.69/33.0 [kV]
Rated power	2.5 [MVA]
Leakage reactance	0.082573 [pu]
Copper losses	0.0084 [pu]
No-load losses	0.0022 [pu]
Wind Farm Transformer Model	
Connection method	Δ / Y / Δ
Voltage	33.0/132.0/33.0 [kV]
Rated power	180.0 [MVA]
Leakage reactance	0.1 [pu]
Copper losses	0.004 [pu]
No-load losses	0.001 [pu]

D. Modeling of DFIG-based Wind Turbine

A complete wind turbine model is used in this study [20]. The model includes the wind speed model, the aerodynamic model of the wind turbine, the mechanical model of the transmission system and models of the electrical components. The induction generator, PWM (Pulse Width Modulated) voltage source converters, transformers, and the control and supervisory system are modeled in details [20].

Fig. 4 illustrates the DFIG-based wind turbine model in ATP [20]. This model is used for accurate simulation of the DFIG-based wind farm. Also, Table 4 summarizes the data used to parameterize the DFIG.

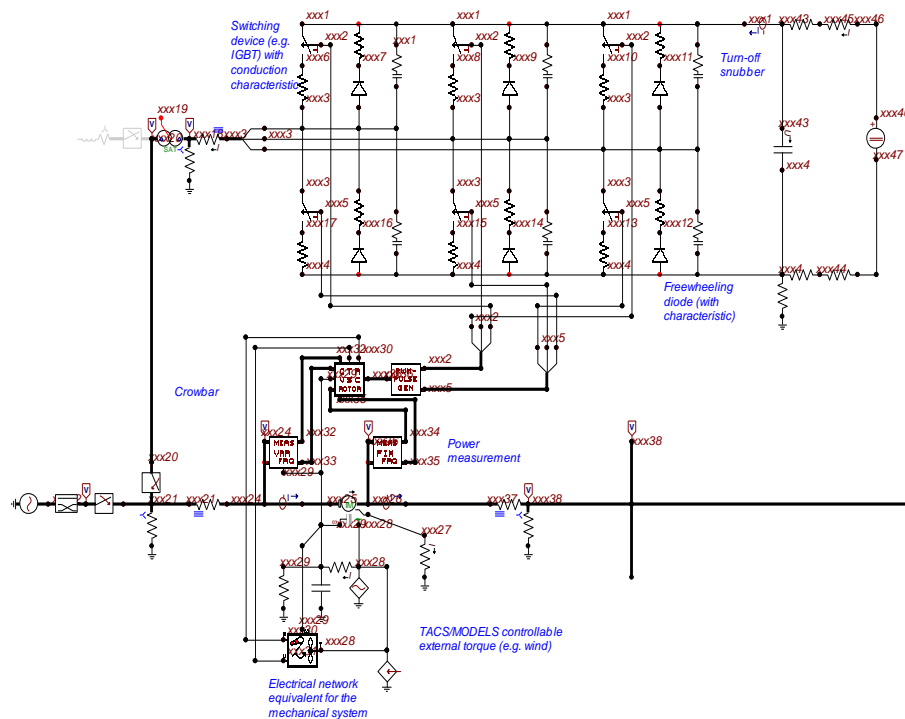


Fig. 4: The DFIG-based wind turbine model in ATP [18]



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

Table 4: Parameters of the DFIG-based wind turbine

Parameter	Value
Stator resistance	0.0025 Ω
Stator leakage inductance	0.097 mH
Magnetization inductance	3 mH
Rotor resistance	0.0083 Ω
Rotor leakage inductance	0.115 mH
Electrical turn ratio	4
Moment of inertia (inertia constant = 2 s.)	2.400 Kg .m ²
Rated apparent power	6.500 KVA

III. SWITCHING OVERVOLTAGE MITIGATION METHODS

A- The Mitigation Methods

Traditionally, SOV is limited through the adoption of PIR in the line circuit breakers. Another method to reduce SOV is the synchronous switching of circuit breakers. The installation of shunt reactors is also used to mitigate SOV. Furthermore, the surge arresters are used to limit SOV in power systems. ATP is used for modeling of the investigated SOV mitigation methods.

Pre-Insertion Resistor (PIR): The closing resistors are inserted in series with the cable, normally being short circuited after 10 ms, thereby damping the switching overvoltage[21]. In the present case, an actual 500 Ω resistor, with an insertion time equals the switching time, is installed.

Synchronized Circuit Breakers: By means of synchronized switching controllers, both energizing and de-energizing operations can be controlled with regard to the point-on-wave position to mitigate harmful transients [22]. The suitable making instant for controlled switching is the time in which the voltage across the circuit breaker contacts for each phase is zero and the predicted time span between the closing instant of the first and the last pole is as small as possible [23]. In this study, the closing order is given when the voltage of each phase crosses consecutive zero.

Shunt Reactor: Shunt reactor is proposed to damp the overvoltages and to keep the system voltage within the permissible limits [24]. Reactors are modeled in many studies by a simple lumped inductor with a series resistance. A parallel resistance may be added for realistic high frequency damping [25]. A shunt reactor is added nearby the switching point.

Surge Arrester: Surge arrester provides a temporal path to earth which the superfluous charge is removed from the system [26]. With the information of volt-ampere characteristic of surge arrester, equivalent model of surge arrester is presented in [27]. This model is used in this study.

B- Results and Discussion

The switching overvoltages, which are generated in wind turbine systems due to switching operations during energization procedures, are evaluated. The investigation of SOV mitigation is studied due to the energization of row A. This is carried out by closing the three phases of the circuit breaker at the platform of row A. The switching is applied at the voltage peak by closing the circuit breaker phases when the voltage of each phase crosses consecutive 90°. The voltage waveforms caused by the switching are investigated on both the HV side (33.0 kV) and the LV side (0.69 kV) of the wind turbine transformers of row A. Figs. 4 to 7 show the maximum SOV at both the HV side and the LV side of the first wind turbine transformer with and without using PIR, controlled switching of circuit breaker, shunt reactor, or surge arresters, respectively.

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

Due to using the PIR, the SOV at the HV side of the wind turbine transformers of row A is reduced from 1.526 pu (29.08 kV) to 1.108 pu (21.1 kV) and from 1.576 pu (1.087 kV) to 1.1965 pu (0.826 kV) at the LV side, as shown in Fig. 4. Fig. 5 illustrates the SOV due to using controlled switching of the circuit breaker at the HV side of the wind turbine transformers of row A which is reduced from 1.5266 pu (29.08 kV) to 0.9929 pu (18.915 kV) and from 1.576 pu (1.087 kV) to 1.124 pu (0.7758 kV) at the LV side.

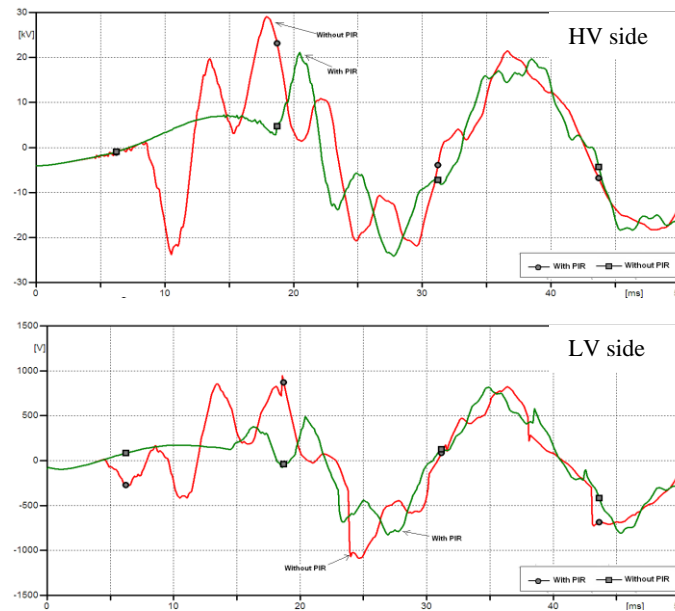


Fig. 4 The SOV at HV and LV sides of wind turbine transformers of row A with and without PIR.

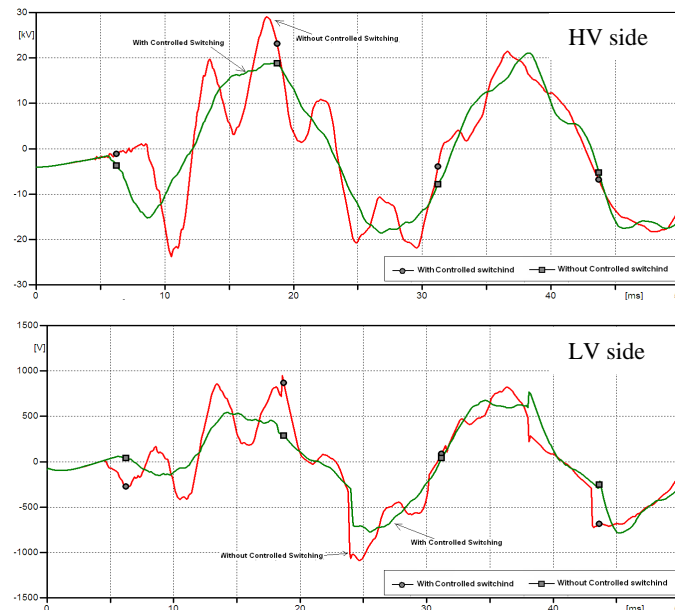


Fig. 5 The SOV at HV and LV sides of wind turbine transformers of row A with and without Controlled C.B

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

Using the shunt reactor reduces the SOV at the HV side of the wind turbine transformers of row A from 1.5266 pu (29.08 kV) to 1.305 pu (24.859 kV) and at the LV side is reduced from 1.576 pu (1.087 kV) to 1.3047 pu (0.9 kV), as shown in Fig. 6. Using the surge arrester reduces the SOV at the HV side of the wind turbine transformers of row A from 1.5266 pu (29.08 kV) to 1.422 pu (27.087 kV) and at the LV side from 1.576 pu (1.087 kV) to 1.126 pu (0.777 kV), as shown in Fig. 7.

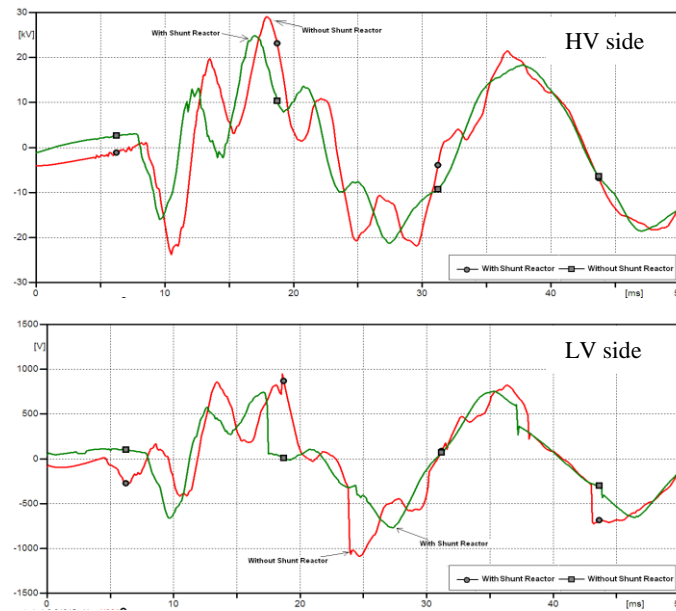


Fig. 6 The SOV at HV and LV sides of wind turbine transformers of row A with and without Shunt Reactor

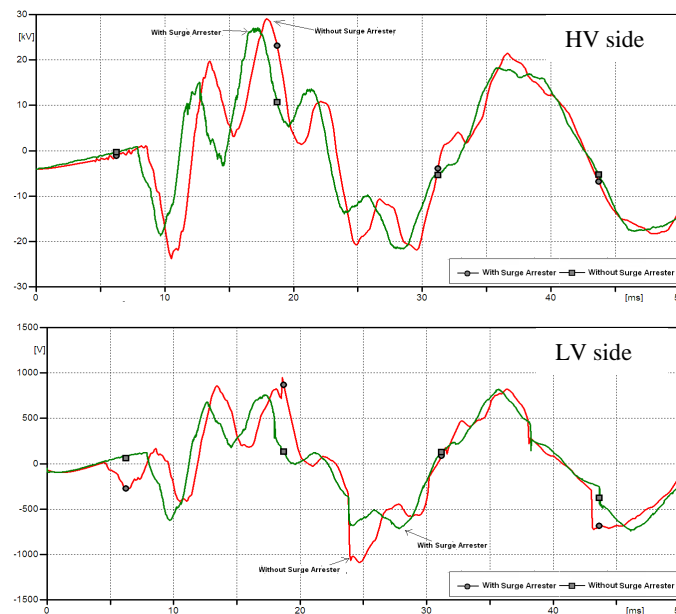


Fig. 7 The SOV at HV and LV sides of wind turbine transformers of row A with and without surge arrester

It can be seen that the PIR and the controlled switching of circuit breaker present an accepted remarkable performance. They reduce the overvoltages to acceptable values (around 1.0 pu).



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 1, January 2014

IV. CONCLUSION

In this paper the mitigation of energization switching overvoltages in weak grid-connected wind farms is investigated. The DFIG-based wind turbine model in ATP is used for the simulation of the wind farm. A wind farm which consists of 72 wind turbines is used for this analysis. The pre-insertion resistor, controlled switching of circuit breaker, shunt reactor, and surge arresters are chosen as protective devices to mitigate the switching overvoltages.

The results show that the switching overvoltages decrease as the PIR or controlled switching of the circuit breaker is used. The shunt reactor and the surge arrestor can't mitigate the switching overvoltages to the accepted levels. The superior the switching overvoltages in the grid-connected offshore wind farm encourages the authors for more investigations on its effects on the DFIG performance.

REFERENCES

- [1] Bindner, H., "Power Control for Wind Turbines in Weak Grids: Concepts Development", Risø National Laboratory, Roskilde, March 1999.
- [2] M. Rashed, S. Abulanwar, F. M. H. Youssef, "H ∞ Robust Controller for a Long VSC-HVDC Link Connected to a Weak Grid", Mansoura Engineering Journal, Vol. 35, No.1, PP.E.53-E.60, March 2010.
- [3] Thukaram, D., Khincha, H. P. and Khandelwa, S., "Estimation of Switching Transient Peak Overvoltages During Transmission Line Energization using Artificial Neural Network", Electric Power Systems Research, Vol. 76, pp. 259–269, 2006.
- [4] Janik, P., Lobos, T. and Rezmer, J., "Assessment of Transients in Power System with Wind Generators by Application of Prony Method", 19th International Conference on Electricity Distribution, CERID, Vienna, 21-24, Paper No 0225, May 2007.
- [5] Intermediate Energy Infobook, "Wind Energy", www.NEED.org, 2012.
- [6] Bickford, J. P. and Heaton, A. G., "Transient Overvoltage on Power Systems", IEE Proceedings, Vol.133, Pt.C, No.4, May 1986.
- [7] GIGRE Working Group, "Switching Overvoltage in EHV and UHV Systems with Special Reference to Closing and Reclosing Transmission Lines", Electra, Vol. 30, pp. 70-122, 1973.
- [8] King, R., Moore, F., Jenkins, N., Haddad, A., Griffiths, H. and Osborne, M., "Switching Transients in Offshore Wind Farms – Impact on the Offshore and Onshore Networks", IPST, Delft, the Netherlands, June 14-17, 2011.
- [9] Zobaa, A. F., "Technology of VAR Compensators for Induction Generator Application in Wind Energy Conversion Systems", Journal of Electrical Systems, Vol.2, No.3, pp.172-184, 2006.
- [10] Pasand, M., Dadashzadeh, M. and Khodayar, M., "Limitation of Transmission Line Switching Overvoltages using Switchsync Relays", IPST, Montreal, Canada, June 19-23, Paper No.087, 2005.
- [11] Tapia, A., Tapia, G., Ostolaza, J. X. and Sáenz, J. R., "Modeling and Control of a Wind Turbine Driven Doubly Fed Induction Generator", IEEE Transactions On Energy Conversion, Vol. 18, No. 2, June 2003.
- [12] Babypriya, B. and Anita, R., "Modeling, Simulation and Analysis of Doubly Fed Induction Generator for Wind Turbines", Journal of Electrical Engineering, Vol. 60, No. 2, pp.79–85, 2009.
- [13] Muñoz, J. C., "Comparative Stability Analysis of DFIG-based Wind Farms and Conventional Synchronous Generators", ece.uwaterloo.ca.
- [14] Prikler, L. and Høidalen, H. K., "ATPDRAW version 5.6 Users' Manual".
- [15] Arana, I., Holbøll, J., Sørensen, T., Nielsen, A. H., Sørensen, P. and Holmstrøm, O., "Comparison of Measured Transient Overvoltages in the Collection Grid of Nysted Offshore Wind Farm with EMT Simulations", IPST, Kyoto, Japan, June 3-6, 2009.
- [16] Badran, E. A., Rizk, M. E. M. and Abdel-Rahman, M. H., "Investigation of Submarine Cable Parameters Impact on Energization Transients in Offshore Wind Farms", IPST, Delft, The Netherlands, June 14-17, Paper No. 182, 2011.
- [17] "ABB XLPE Cables User's Guide", Technical documentation, www.abb.com.
- [18] Chiesa, N. and Høidalen, H. K., "Hysteretic iron-core inductor for transformer inrush current modeling in EMT", 16th Power Systems Computation Conference, PSCC08, Glasgow, Scotland, Jul. 2008.
- [19] Hassan, E. O., Badran, E. A. and Youssef, F. M. H., "A Comparison Between Some Currently Used High Frequency Transformer Models", Mansoura Engineering Journal, Vol. 39, No. 1, pp. E1-E7, March 2013.
- [20] La Seta, P., "Modeling and Control of Wind Turbines Based on Doubly-Fed Induction Generators (DFIG)", EEUG Meeting, 2009.
- [21] Soloot, A. H., Gholami, A., Agheb, E., Shorbendaeipour, A. and Molchhari, P., "Investigation of Transmission line Over Voltages and Their Deduction Approach", Word Academt of Science Engineering and Technology, Vol. 53, pp. 18-26, 2009.
- [22] Sanaye-Pasand, M., Dadashzadeh, M. R. and Khodayar, M., "Limitation of Transmission Line Switching Overvoltages using Switchsync Relays", IPST, Montreal, Canada, June 19-23, Paper No. IPST05 – 087, 2005.
- [23] Dantas, K. M. C., Neves, W. L. A., Fernandes, D., Cardoso, G. A. and Fonseca, L. C., "On Applying Controlled Switching to Transmission Lines: Case Studies", IPST2009, Kyoto, Japan, June 3-6, 2009.
- [24] Elkhodary, S. M. and Abdel-Munem, A. S., "New Proposed Method of Damping Temporary Overvoltages on Power System Interconnections", Journal of American Science, Vol. 6, No. 11, pp. 336-342, 2010.
- [25] The Switching Transients Task Force of the IEEE Modeling and Analysis of System Transients Working Group, "Modeling Guidelines for Switching Transients", www.ee.umanitoba.ca.
- [26] Xue, H., "Analysis of Switching Transient Overvoltage in the Power System of Floating Production Storage and Offloading Vessel", M.Sc. Thesis, Delft University of Technology.
- [27] Bayadi, A., Harid, N., Zehar, K. and Belkhiat, S., "Simulation of Metal Oxide Surge Arrester Dynamic Behavior Under Fast Transients", IPST, New Orleans, USA, 2003.